

**NATIONAL EXAMINATIONS DECEMBER 2009**

**04-BS-2**

**PROBABILITY AND STATISTICS**

**2 HOURS DURATION**

**NOTES:**

1. If doubt exists as to the interpretation of any question, the candidate is urged to submit with the answer paper a clear statement of any assumption made.
2. "Closed Book" – no-aids other than
  - (i) A Casio or Sharp approved calculator
  - (ii) ONE hand-written information sheet (8.5"x11"), filled on both sides.
3. Any 5 questions constitute a complete paper. Only 5 questions will be marked.
4. All questions are of equal value.
5. Statistical tables of the normal, t, chi-square and F distributions are provided.

**Marking Scheme**

- 1.(a) 5 marks (b) 5 marks (c) 5 marks (d) 5 marks
- 2.(a) 5 marks (b) 5 marks (c) 5 marks (d) 5 marks
- 3.(A) 5 marks (B) 5 marks (C) (a) 5 marks (b) 5 marks
- 4.(a) 6 marks (b) 4 marks (c) 5 marks (d) 5 marks
- 5.(a) 5 marks (b) 5 marks (c) 5 marks (d) 5 marks
6. 20 marks
- 7.(a) 10 marks (b) 10 marks
- 8.(a) 5 marks (b) 5 marks (c) 5 marks (d) 5 marks

1. The useful life  $X$  of a drill bit widely used in the production line of the automotive industry is a normally distributed random variable with mean and standard deviation equal to 1,880 hours and 100 hours respectively.

- (a) If a worker replaces an old bit with a new one what is the probability that the useful life of the new bit will exceed 1,800 hours? Draw the probability density function of  $X$ , neatly and clearly, and indicate the area that corresponds to this probability.
- (b) Another worker replaces an old bit with a new one in another section of the production line. What is the probability that the useful life of this bit will differ from the mean by less than 130 hours? Draw the probability density function of  $X$ , clearly and neatly, and indicate the area that corresponds to this probability.
- (c) Let  $M$  represent the mean useful life of a random sample of 16 bits. (i) Find the mean and standard deviation of  $M$ . (ii) Write down the probability density function of  $X$  and  $M$ . (iii) Draw the probability density function of  $X$  and  $M$  on the same diagram. (iv) Compute the probability that  $M$  exceeds 1,920 hours.
- (d) Let  $T$  be the sum of the useful life of 36 bits. Find  $E(T)$  and  $\text{Var}(T)$ . Then compute the probability that  $T$  exceeds 68,000 hours.

2. Extensive data gathered by the senior manager of the Continental Motor League (CML) revealed that 20% of the calls received by the Service Centre concerned a flat tire.

- (a) Compute the probability that in a random sample of 14 calls more than 2 but fewer than 6 concern a flat tire.
- (b) Compute the probability that in a random sample of 12 calls more than four concern a flat tire.
- (c) Assume now that the Service Centre of CML received 1,800 calls in a given week. Use an appropriate approximation to find the probability that at least 340 calls concerned a flat tire.
- (d) Compute the probability that in a random sample of 15 calls more than eleven do not concern a flat tire.

3.(A) Mr. Goodman, the owner of Homebuddy Hardware, receives a lot of eighteen toasters from Friendly Kitchen Appliances. Unknown to Mr. Goodman, eight toasters are substandard. If nine toasters were sold at random what is the probability that at least five were substandard?

3.(B) The design office of a medium-sized engineering company is made up of five civil engineers, nine mechanical engineers and six electrical engineers. A committee is to be formed by randomly selecting six members from the design office. What is the probability that more than two civil engineers will be in the committee?

3.(C) The number of particles emitted from a radioactive source in  $t$  seconds follows the Poisson distribution with mean  $t/30$ .

- (a) Find the probability that in a period of one minute (i) no particle and (ii) at least four particles will be emitted.
- (b) Use an appropriate approximation to find the probability that fewer than 130 particles will be emitted in one hour.

4. An extensive survey gathered by the general manager of the transit commission of a large urban centre revealed that 40% of the working adults live in municipality  $M_1$ , 25% in municipality  $M_2$ , 20% in municipality  $M_3$  while the remaining 15% live in municipality  $M_4$ . The same survey also revealed that 70% of the working adults living in municipality  $M_1$  use public transportation to commute to work, while the corresponding numbers for municipalities  $M_2$ ,  $M_3$  and  $M_4$  were 75%, 60% and 50% respectively.

- (a) Let  $T$  represent the event “working adult uses public transportation”. Also let  $T_C$  represent the complement of  $T$ . Draw a neat tree diagram indicating all the relevant probabilities using the symbols  $M_1$ ,  $M_2$ ,  $M_3$ ,  $M_4$ ,  $T$  and  $T_C$ .
- (b) Compute the following probabilities:
  - (i)  $\Pr(T)$  ; (ii)  $\Pr(M_3 \cap T)$  ; (iii)  $\Pr(M_2 \cap T_C)$
- (c) Assume that a working adult is randomly selected from the entire urban population and it is found that this person uses public transportation to commute to work. What is the probability that this person lives in municipality  $M_1$ ?
- (d) Assume now that 8 working adults are randomly selected from the entire urban population. What is the probability that at least 6 use public transportation?

5. Consider the probability density function  $f(x)$  of the random variable  $X$  described below.

- (a) Find the value of  $K$ . Then sketch, clearly and neatly,  $f(x)$  against  $x$ .
- (b) Find the expectation of  $X$ .
- (c) Compute the variance of  $X$ .
- (d) Find the cumulative distribution function  $F(x)$ . Then sketch, clearly and neatly,  $F(x)$  against  $x$ .

$$f(x) = \begin{cases} K / x^4 & 1 \leq x \\ \text{otherwise} & 0 \end{cases}$$

6. The following table displays the number of employees and the number of minor accidents occurring in a year in four manufacturing concerns:

	MANUFACTURER			
	A	B	C	D
Number of employees	4,000	3,000	1,000	2,000
Number of accidents	23	14	10	17

Test the hypothesis that the expected number of minor accidents is proportional to the number of employees working in each concern. Let  $\alpha=0.05$ .

7. Tests were made by the Research and Development department of Major Motors Corporation (MMC) to determine the performance of cars, in kilometres per litre, using two different gasoline additives. Originally thirty nominally identical cars took part in this experiment, fifteen using gasoline with Additive A and the other fifteen using gasoline with Additive B. However, due to some clerical errors, three results had to be discarded. The remaining results of these tests were as follows:

	Additive A	Additive B
Sample size	$n_A = 14$	$n_B = 13$
Sample Mean	$m_A = 13.4$	$m_B = 14.0$
Sample Standard Deviation	$s_A = 0.70$	$s_B = 0.85$

- (a) Does this data indicate that the variability of the performance of cars obtained with Additive A is significantly different from the one obtained with Additive B? Let  $\alpha=0.05$ . State any assumptions you need to make.
- (b) Test the hypothesis that the mean performance of cars obtained with Additive A is not significantly different from that obtained with Additive B. Let  $\alpha=0.05$ .

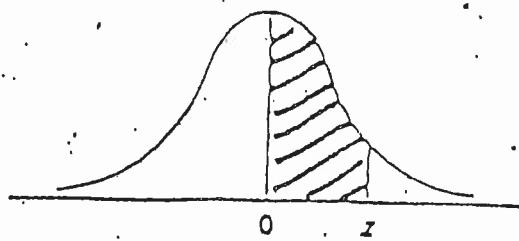
8. In the following data Y represents the population (in millions) of an urban centre while X represents the number of outside workers (in thousands) employed by the municipality of this centre.

$$\sum_{i=1}^n X_i = 82 \quad ; \quad \sum_{i=1}^n X_i^2 = 326 \quad ; \quad \sum_{i=1}^n Y_i = 191.0$$

$$\sum_{i=1}^n Y_i^2 = 1794.0 \quad ; \quad \sum_{i=1}^n X_i Y_i = 753.0 \quad ; \quad n=23$$

- (a) Compute the  $\text{Cov}(X, Y)$  and the coefficient of correlation  $r$ .
- (b) Test the hypothesis that the true coefficient of correlation  $\rho$  is not significantly different from 0.9.

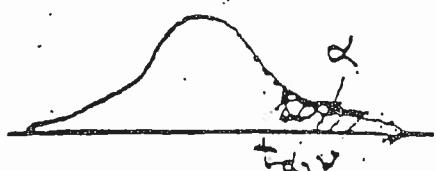
- (c) It is believed that Y and X are related by an equation of the form  $Y = \beta_0 + \beta_1 X + \varepsilon$ . Write down the normal equations of the least squares line and then compute the estimates  $b_0$  and  $b_1$  of  $\beta_0$  and  $\beta_1$  respectively.
- (d) Compute the error sum of squares then use this information to find the 95% confidence limits of  $\beta_1$ .

NORMAL DISTRIBUTION TABLE

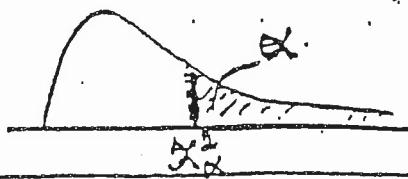
$$F(z) = \frac{1}{\sqrt{2\pi}} \int_0^z e^{-t^2/2} dt$$

<i>z</i>	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
0.0	.0000	.0040	.0080	.0120	.0160	.0199	.0239	.0279	.0319	.0359
0.1	.0398	.0438	.0478	.0517	.0557	.0596	.0636	.0675	.0714	.0753
0.2	.0793	.0832	.0871	.0910	.0948	.0987	.1026	.1064	.1103	.1141
0.3	.1179	.1217	.1255	.1293	.1331	.1368	.1405	.1443	.1480	.1517
0.4	.1554	.1591	.1628	.1664	.1700	.1736	.1772	.1808	.1844	.1879
0.5	.1915	.1950	.1985	.2019	.2054	.2088	.2123	.2157	.2190	.2224
0.6	.2257	.2291	.2324	.2357	.2389	.2422	.2454	.2486	.2517	.2549
0.7	.2580	.2611	.2642	.2673	.2704	.2734	.2764	.2794	.2823	.2852
0.8	.2881	.2910	.2939	.2957	.2995	.3023	.3051	.3078	.3106	.3133
0.9	.3159	.3186	.3212	.3238	.3264	.3289	.3315	.3340	.3365	.3389
1.0	.3413	.3438	.3461	.3485	.3508	.3531	.3554	.3577	.3599	.3621
1.1	.3643	.3665	.3686	.3708	.3729	.3749	.3770	.3790	.3810	.3830
1.2	.3849	.3869	.3888	.3907	.3925	.3944	.3962	.3980	.3997	.4015
1.3	.4032	.4049	.4066	.4082	.4099	.4115	.4131	.4147	.4162	.4177
1.4	.4192	.4207	.4222	.4236	.4251	.4265	.4279	.4292	.4306	.4319
1.5	.4332	.4345	.4357	.4370	.4382	.4394	.4406	.4418	.4429	.4441
1.6	.4452	.4463	.4474	.4484	.4495	.4505	.4515	.4525	.4535	.4545
1.7	.4554	.4564	.4573	.4582	.4591	.4599	.4608	.4616	.4625	.4633
1.8	.4641	.4649	.4656	.4664	.4671	.4678	.4686	.4693	.4699	.4706
1.9	.4713	.4719	.4726	.4732	.4738	.4744	.4750	.4756	.4761	.4767
2.0	.4772	.4778	.4783	.4788	.4793	.4798	.4803	.4808	.4812	.4817
2.1	.4821	.4826	.4830	.4834	.4838	.4842	.4846	.4850	.4854	.4857
2.2	.4861	.4864	.4868	.4871	.4875	.4878	.4881	.4884	.4887	.4890
2.3	.4893	.4895	.4898	.4901	.4904	.4906	.4909	.4911	.4913	.4916
2.4	.4918	.4920	.4922	.4925	.4927	.4929	.4931	.4932	.4934	.4936
2.5	.4938	.4940	.4941	.4943	.4945	.4946	.4948	.4949	.4951	.4952
2.6	.4953	.4955	.4956	.4957	.4959	.4960	.4961	.4962	.4963	.4964
2.7	.4965	.4966	.4967	.4968	.4969	.4970	.4971	.4972	.4973	.4974
2.8	.4974	.4975	.4976	.4977	.4977	.4978	.4979	.4979	.4980	.4981
2.9	.4981	.4982	.4982	.4983	.4984	.4984	.4985	.4985	.4986	.4986
3.0	.4987	.4987	.4987	.4988	.4988	.4989	.4989	.4989	.4990	.4990

## t - DISTRIBUTION

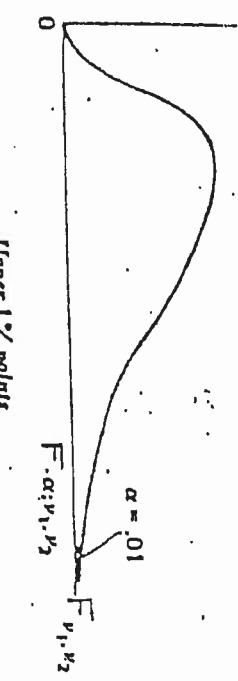


$\nu$	$\alpha = 0.100$	$\alpha = 0.050$	$\alpha = 0.025$	$\alpha = 0.010$	$\alpha = 0.005$	$\nu$
1	3.078	6.314	12.706	31.821	53.657	1
2	1.886	2.920	4.303	5.965	9.925	2
3	1.538	2.353	3.182	4.541	5.841	3
4	1.523	2.132	2.776	3.747	4.604	4
5	1.476	2.015	2.571	3.365	4.032	5
6	1.440	1.943	2.447	3.143	3.707	6
7	1.415	1.895	2.365	2.998	3.499	7
8	1.397	1.860	2.306	2.896	3.355	8
9	1.383	1.831	2.252	2.821	3.250	9
10	1.372	1.812	2.228	2.764	3.169	10
11	1.363	1.796	2.201	2.718	3.106	11
12	1.356	1.782	2.179	2.681	3.055	12
13	1.350	1.771	2.150	2.650	3.012	13
14	1.345	1.761	2.145	2.624	2.977	14
15	1.341	1.753	2.131	2.602	2.947	15
16	1.337	1.746	2.120	2.583	2.921	16
17	1.333	1.740	2.110	2.567	2.898	17
18	1.330	1.734	2.101	2.552	2.878	18
19	1.328	1.729	2.093	2.539	2.861	19
20	1.325	1.725	2.086	2.528	2.845	20
21	1.323	1.721	2.080	2.518	2.831	21
22	1.321	1.717	2.074	2.508	2.819	22
23	1.319	1.714	2.069	2.500	2.807	23
24	1.318	1.711	2.064	2.492	2.797	24
25	1.316	1.708	2.060	2.485	2.787	25
26	1.315	1.706	2.056	2.479	2.779	26
27	1.314	1.703	2.052	2.473	2.771	27
28	1.313	1.701	2.048	2.467	2.763	28
29	1.311	1.699	2.045	2.462	2.756	29
30	1.282	1.645	1.950	2.326	2.576	30

THE CHI-SQUARE DISTRIBUTION

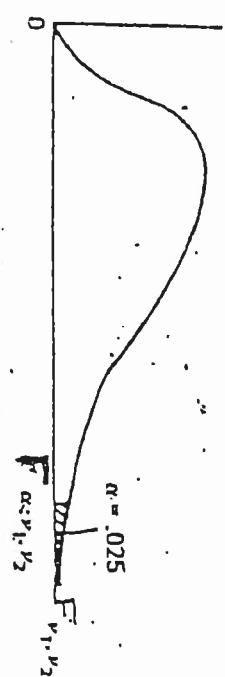
$\chi^2$	Probability that chi-square value will be exceeded							
	.995	.990	.975	.950	.050	.025	.010	.005
1	---	---	---	.004	3.84	5.02	6.63	7.88
2	.01	.02	.05	.10	5.99	7.38	9.21	10.60
3	.07	.11	.22	.35	7.81	9.35	11.34	12.64
4	.21	.30	.48	.71	9.49	11.14	13.28	14.86
5	.41	.55	.83	1.15	11.07	12.83	15.09	16.75
6	.68	.87	1.24	1.64	12.59	14.45	16.91	18.55
7	.99	1.24	1.69	2.17	14.07	16.01	18.48	20.28
8	1.34	1.65	2.18	2.73	15.51	17.53	20.09	21.96
9	1.73	2.09	2.70	3.33	16.92	19.02	21.57	23.59
10	2.16	2.56	3.25	3.94	18.31	20.48	23.21	25.19
11	2.60	3.05	3.52	4.57	19.68	21.92	24.72	26.76
12	3.07	3.57	4.40	5.23	21.03	23.34	26.22	23.30
13	3.57	4.11	5.01	5.89	22.36	24.74	27.69	29.82
14	4.07	4.66	5.63	6.57	23.68	26.12	29.14	31.32
15	4.60	5.23	6.26	7.26	25.00	27.49	30.58	32.80
16	5.14	5.81	6.91	7.96	26.30	28.85	32.00	34.27
17	5.70	6.41	7.56	8.67	27.59	30.19	33.41	35.72
18	6.26	7.01	8.23	9.39	28.87	31.53	34.81	37.16
19	6.84	7.63	8.91	10.12	30.14	32.65	36.19	38.58
20	7.43	8.26	9.59	10.85	31.41	34.17	37.57	40.00
21	8.03	8.90	10.28	11.59	32.67	35.48	38.53	41.40
22	8.64	9.54	10.98	12.34	33.92	36.78	40.29	42.80
23	9.25	10.20	11.69	13.09	35.17	38.08	41.64	44.18
24	9.89	10.86	12.40	13.85	36.42	39.36	42.98	45.55
25	10.52	11.52	13.12	14.61	37.65	40.65	44.31	46.93
26	11.16	12.20	13.84	15.38	38.89	41.92	45.64	48.25
27	11.81	12.88	14.57	16.15	40.11	43.19	46.96	49.64
28	12.46	13.56	15.31	15.93	41.34	44.46	48.23	50.95
29	13.12	14.25	16.05	17.71	42.56	45.72	49.59	52.31
30	13.79	14.95	16.79	18.49	43.77	46.98	50.89	53.6
40	20.71	22.16	24.43	26.51	55.76	59.34	63.69	66.7
50	27.99	29.71	32.36	34.76	67.50	71.42	76.15	79.4
60	35.53	37.48	40.48	43.19	79.08	83.30	88.33	91.9
70	43.28	45.44	48.76	51.74	90.53	95.02	100.43	104.2
80	51.17	53.54	57.15	60.39	101.88	106.63	112.33	116.3
90	59.20	61.75	65.65	69.13	113.14	118.14	124.12	128.3
100	67.33	70.06	74.22	77.93	124.34	129.56	135.81	140.0

## F - DISTRIBUTION



$v_1$	1	2	3	4	5	6	7	8	9	10	12	15	20	24	30	40	60	120	*
1	4052	4899.5	3403	3625	3764	3859	3928	3982	4022	4056	4106	4157	4209	4255	4361	4287	4313	4339	4366
2	98.50	99.00	99.17	99.25	99.30	99.33	99.36	99.37	99.39	99.40	99.42	99.43	99.46	99.47	99.48	99.49	99.50	99.50	99.50
3	34.12	30.82	29.46	28.71	28.24	27.91	27.67	27.49	27.33	27.23	27.05	26.87	26.69	26.50	26.41	26.32	26.22	26.13	26.13
4	21.20	18.00	16.69	15.98	15.32	15.21	14.98	14.80	14.65	14.57	14.37	14.20	14.02	13.91	13.84	13.75	13.65	13.56	13.46
5	16.26	13.27	12.06	11.39	10.97	10.67	10.46	10.29	10.16	10.05	9.89	9.72	9.55	9.47	9.38	9.29	9.20	9.11	9.02
6	13.75	10.92	9.78	9.15	8.75	8.47	8.26	8.10	7.98	7.87	7.72	7.56	7.40	7.31	7.23	7.14	7.06	6.97	6.88
7	12.25	9.35	8.45	7.85	7.46	7.19	6.99	6.84	6.72	6.62	6.47	6.31	6.16	6.07	5.91	5.75	5.56	5.36	5.12
8	11.26	8.63	7.59	7.01	6.63	6.37	6.18	6.03	5.91	5.81	5.67	5.51	5.35	5.26	5.11	4.96	4.81	4.73	4.65
9	10.36	8.02	6.99	6.42	6.06	5.80	5.61	5.47	5.35	5.26	5.11	4.96	4.81	4.73	4.65	4.57	4.48	4.40	4.31
10	10.04	7.36	6.55	5.99	5.64	5.39	5.20	5.06	4.94	4.85	4.71	4.56	4.41	4.33	4.25	4.17	4.08	4.00	3.91
11	9.63	7.21	6.22	5.67	5.32	5.07	4.80	4.74	4.63	4.54	4.40	4.25	4.10	4.02	3.94	3.86	3.78	3.69	3.60
12	9.33	6.93	5.95	5.41	5.06	4.82	4.64	4.50	4.39	4.29	4.16	4.01	3.86	3.78	3.70	3.62	3.54	3.45	3.35
13	9.07	6.70	5.74	5.21	4.86	4.62	4.44	4.30	4.19	4.09	3.96	3.82	3.66	3.59	3.51	3.43	3.37	3.27	3.18
14	8.86	6.51	5.56	5.04	4.69	4.46	4.28	4.14	4.01	3.94	3.80	3.67	3.57	3.49	3.41	3.33	3.26	3.19	3.10
15	8.68	6.36	5.42	4.89	4.56	4.32	4.14	4.00	3.89	3.80	3.67	3.52	3.42	3.33	3.24	3.16	3.09	3.02	2.93
16	8.53	6.23	5.29	4.77	4.44	4.20	3.99	3.78	3.69	3.55	3.41	3.26	3.16	3.08	2.99	2.93	2.85	2.75	2.65
17	8.40	6.11	5.18	4.67	4.34	4.10	3.93	3.79	3.68	3.59	3.46	3.31	3.16	3.08	2.99	2.92	2.84	2.75	2.67
18	8.29	6.01	5.09	4.58	4.25	4.01	3.84	3.71	3.60	3.51	3.37	3.23	3.08	3.00	2.92	2.84	2.76	2.67	2.58
19	8.18	5.91	5.01	4.50	4.17	3.94	3.77	3.63	3.52	3.41	3.30	3.15	3.03	2.92	2.84	2.76	2.67	2.59	2.50
20	8.10	5.85	4.94	4.43	4.10	3.87	3.70	3.56	3.46	3.37	3.23	3.09	2.94	2.86	2.78	2.69	2.61	2.52	2.42
21	8.02	5.78	4.87	4.37	4.04	3.81	3.64	3.51	3.40	3.31	3.17	3.03	2.88	2.80	2.72	2.64	2.55	2.46	2.36
22	7.95	5.72	4.82	4.31	3.99	3.76	3.59	3.45	3.35	3.26	3.12	2.98	2.83	2.75	2.67	2.58	2.49	2.42	2.33
23	7.88	5.66	4.76	4.26	3.94	3.71	3.54	3.41	3.30	3.21	3.03	2.93	2.78	2.66	2.58	2.49	2.40	2.31	2.21
24	7.82	5.61	4.72	4.22	3.90	3.67	3.50	3.36	3.26	3.17	3.03	2.91	2.79	2.66	2.58	2.49	2.40	2.31	2.21
25	7.77	5.57	4.68	4.18	3.85	3.63	3.46	3.32	3.18	3.09	2.96	2.81	2.66	2.58	2.50	2.42	2.33	2.22	2.13
26	7.72	5.53	4.64	4.14	3.82	3.59	3.42	3.29	3.18	3.09	2.96	2.81	2.66	2.58	2.50	2.42	2.33	2.22	2.10
27	7.68	5.49	4.60	4.11	3.78	3.56	3.39	3.26	3.15	3.06	2.93	2.78	2.63	2.55	2.47	2.38	2.29	2.20	2.10
28	7.64	5.45	4.57	4.07	3.75	3.53	3.36	3.23	3.12	3.03	2.90	2.75	2.60	2.52	2.44	2.35	2.26	2.17	2.06
29	7.60	5.42	4.54	4.04	3.73	3.50	3.33	3.20	3.09	3.00	2.87	2.73	2.57	2.49	2.41	2.33	2.23	2.14	2.03
30	7.56	5.39	4.51	4.02	3.70	3.47	3.30	3.17	3.07	2.98	2.84	2.70	2.55	2.47	2.39	2.30	2.21	2.11	2.01
31	7.51	5.18	4.31	3.83	3.51	3.29	3.12	2.99	2.89	2.80	2.66	2.52	2.37	2.29	2.20	2.11	2.02	1.92	1.80
32	7.48	4.98	4.11	3.54	3.21	2.95	2.82	2.72	2.63	2.55	2.37	2.20	2.03	1.94	1.84	1.73	1.66	1.59	1.47
33	7.35	4.79	3.95	3.17	2.96	2.79	2.66	2.55	2.37	2.29	2.20	2.12	2.03	1.94	1.84	1.73	1.58	1.47	1.32
34	7.00	4.60	3.65	3.12	2.95	2.82	2.66	2.55	2.37	2.29	2.20	2.12	2.03	1.95	1.86	1.76	1.66	1.59	1.47
35	6.80	4.49	3.45	2.95	2.82	2.66	2.55	2.37	2.29	2.20	2.12	2.03	1.95	1.86	1.76	1.66	1.59	1.47	1.32
36	6.63	4.35	3.34	2.82	2.70	2.55	2.44	2.35	2.25	2.17	2.09	2.00	1.91	1.82	1.73	1.64	1.55	1.47	1.32
37	6.53	4.21	3.22	2.70	2.58	2.44	2.33	2.23	2.13	2.05	1.96	1.87	1.78	1.69	1.60	1.51	1.42	1.33	1.24
38	6.41	4.11	3.12	2.60	2.48	2.35	2.24	2.14	2.04	1.95	1.86	1.77	1.68	1.59	1.50	1.41	1.32	1.23	1.14

## F - DISTRIBUTION

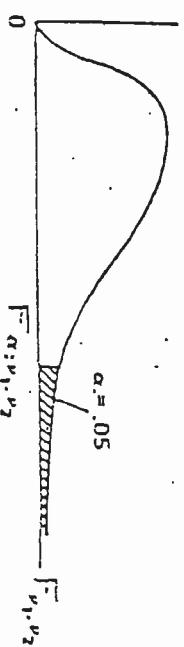


Upper 2.5% point

 $\alpha = .025$  $F_{\alpha; \nu_1, \nu_2}$ 

$\nu_2$	1	2	3	4	5	6	7	8	9	10	12	15	20	24	30	40	60	120	∞
$\nu_1$	647.8	799.5	864.2	899.6	921.8	937.1	948.2	956.7	963.3	968.6	976.7	984.9	993.1	997.2	1001	1006	1010	1014	1018
1	38.51	39.00	39.17	39.25	39.30	39.33	39.36	39.37	39.39	39.40	39.41	39.43	39.45	39.46	39.47	39.48	39.49	39.50	
2	17.44	16.04	15.44	15.10	14.88	14.73	14.62	14.54	14.47	14.42	14.35	14.25	14.17	14.12	14.08	14.04	13.99	13.93	
3	12.22	10.65	9.98	9.60	9.36	9.20	9.07	8.98	8.90	8.84	8.75	8.66	8.56	8.46	8.36	8.21	8.09	8.00	
4	10.01	8.43	7.76	7.39	7.13	6.98	6.83	6.76	6.68	6.62	6.52	6.43	6.33	6.23	6.18	6.12	6.07	6.00	
5	8.81	7.26	6.60	6.23	5.92	5.82	5.70	5.60	5.52	5.46	5.37	5.27	5.17	5.12	5.07	5.01	4.96	4.90	
6	8.07	6.54	5.89	5.52	5.29	5.12	4.99	4.90	4.82	4.76	4.67	4.57	4.47	4.42	4.36	4.31	4.25	4.20	
7	7.57	6.06	5.42	5.05	4.82	4.63	4.51	4.41	4.36	4.30	4.20	4.10	4.00	3.95	3.89	3.78	3.73	3.70	
8	7.21	5.71	5.08	4.72	4.48	4.32	4.20	4.10	4.03	3.96	3.87	3.77	3.67	3.61	3.56	3.51	3.45	3.40	
9	6.94	5.46	4.83	4.47	4.24	4.07	3.95	3.85	3.78	3.72	3.62	3.52	3.42	3.37	3.26	3.20	3.14	3.10	
10	6.70	5.16	4.63	4.28	4.04	3.88	3.76	3.66	3.59	3.53	3.41	3.33	3.23	3.17	3.06	3.00	2.94	2.91	
11	6.72	5.16	4.63	4.28	4.04	3.89	3.77	3.64	3.51	3.44	3.37	3.28	3.18	3.07	3.02	2.96	2.85	2.82	
12	6.35	5.10	4.47	4.12	3.89	3.77	3.60	3.48	3.39	3.31	3.25	3.13	3.05	2.93	2.89	2.84	2.78	2.72	
13	6.41	4.97	4.35	4.00	3.77	3.66	3.50	3.38	3.29	3.21	3.15	3.05	2.95	2.84	2.79	2.73	2.67	2.55	
14	6.30	4.86	4.24	3.89	3.66	3.50	3.38	3.29	3.21	3.15	3.05	2.95	2.84	2.79	2.73	2.67	2.61	2.55	
15	6.77	4.77	4.15	3.80	3.58	3.41	3.29	3.20	3.12	3.06	2.96	2.86	2.76	2.70	2.64	2.59	2.52	2.46	
16	6.12	4.69	4.08	3.73	3.50	3.34	3.22	3.12	3.05	2.99	2.89	2.79	2.68	2.61	2.57	2.51	2.45	2.39	
17	6.04	4.62	4.01	3.66	3.44	3.28	3.16	3.06	2.98	2.92	2.82	2.72	2.62	2.56	2.50	2.44	2.38	2.32	
18	5.98	4.56	3.95	3.61	3.38	3.22	3.10	3.01	2.93	2.87	2.77	2.67	2.56	2.50	2.44	2.38	2.32	2.26	
19	5.92	4.51	3.90	3.56	3.33	3.17	3.05	2.96	2.88	2.82	2.72	2.62	2.51	2.45	2.39	2.33	2.27	2.20	
20	5.87	4.46	3.86	3.51	3.29	3.13	3.01	2.91	2.84	2.77	2.68	2.57	2.46	2.35	2.29	2.24	2.18	2.10	
21	5.83	4.42	3.82	3.48	3.23	3.09	2.97	2.87	2.80	2.73	2.64	2.53	2.42	2.37	2.31	2.25	2.19	2.12	
22	5.79	4.38	3.78	3.44	3.22	3.03	2.93	2.84	2.76	2.70	2.60	2.50	2.39	2.32	2.27	2.21	2.16	2.10	
23	5.75	4.33	3.75	3.41	3.18	3.02	2.90	2.81	2.73	2.67	2.57	2.47	2.36	2.30	2.24	2.18	2.12	2.06	
24	5.72	4.32	3.72	3.38	3.13	2.99	2.87	2.78	2.70	2.64	2.54	2.44	2.33	2.27	2.21	2.15	2.08	2.01	
25	5.69	4.27	3.69	3.35	3.11	2.97	2.85	2.75	2.68	2.61	2.51	2.41	2.30	2.24	2.18	2.12	2.05	1.98	
26	5.66	4.27	3.67	3.33	3.10	2.94	2.82	2.73	2.65	2.59	2.49	2.39	2.29	2.22	2.16	2.10	2.03	1.95	
27	5.63	4.24	3.63	3.31	3.08	2.92	2.80	2.71	2.63	2.57	2.47	2.36	2.26	2.21	2.14	2.08	2.02	1.93	
28	5.61	4.22	3.63	3.29	3.06	2.90	2.78	2.69	2.61	2.53	2.43	2.34	2.22	2.17	2.11	2.05	1.98	1.91	
29	5.59	4.20	3.61	3.27	3.04	2.88	2.76	2.67	2.59	2.51	2.43	2.32	2.21	2.15	2.09	2.03	1.96	1.89	
30	5.57	4.18	3.59	3.25	3.03	2.87	2.75	2.65	2.57	2.51	2.41	2.30	2.24	2.18	2.12	2.05	1.98	1.91	
40	5.42	4.05	3.46	3.13	2.90	2.74	2.62	2.53	2.45	2.39	2.29	2.22	2.16	2.09	2.03	2.01	1.94	1.87	
60	5.29	3.34	3.01	2.79	2.63	2.51	2.39	2.29	2.17	2.06	1.94	1.88	1.82	1.76	1.69	1.63	1.57	1.51	
120	5.13	3.23	2.89	2.52	2.39	2.30	2.22	2.16	2.05	1.94	1.82	1.76	1.69	1.63	1.57	1.51	1.45	1.40	
∞	5.02	3.12	2.57	2.41	2.19	2.05	1.94	1.83	1.71	1.64	1.57	1.48	1.40	1.33	1.27	1.20	1.14	1.08	

## F - DISTRIBUTION



$\nu_1$	1	2	3	4	5	6	7	8	9	10	12	15	20	24	30	40	60	120	∞
1	161.4	199.5	215.7	224.6	210.2	234.0	216.8	218.9	240.5	241.9	241.9	245.9	248.0	249.1	250.2	251.1	252.2	253.3	254.4
2	18.51	19.00	19.16	19.23	19.30	19.33	19.35	19.38	19.40	19.41	19.41	19.43	19.45	19.45	19.46	19.47	19.48	19.49	19.50
3	10.13	9.33	9.28	9.12	9.01	8.94	8.83	8.81	8.79	8.74	8.70	8.66	8.64	8.62	8.59	8.57	8.55	8.53	8.51
4	7.71	6.94	6.39	6.19	6.26	6.16	6.09	6.04	5.96	5.91	5.86	5.80	5.77	5.72	5.69	5.66	5.63	5.60	5.58
5	6.61	5.79	5.41	5.19	5.03	4.95	4.88	4.82	4.77	4.74	4.68	4.62	4.56	4.53	4.50	4.46	4.43	4.40	4.36
6	5.99	5.14	4.76	4.53	4.39	4.28	4.21	4.15	4.10	4.06	3.94	3.87	3.84	3.81	3.77	3.74	3.70	3.67	3.63
7	5.59	4.74	4.35	4.12	3.97	3.87	3.79	3.73	3.68	3.64	3.60	3.53	3.44	3.39	3.28	3.22	3.15	3.12	3.09
8	5.12	4.46	4.07	3.84	3.69	3.58	3.50	3.44	3.39	3.35	3.30	3.23	3.18	3.14	3.07	3.01	2.94	2.86	2.83
9	5.12	4.26	3.86	3.63	3.48	3.37	3.29	3.23	3.18	3.14	3.10	3.07	3.01	2.94	2.89	2.79	2.75	2.73	2.71
10	4.96	4.10	3.71	3.48	3.33	3.22	3.14	3.07	3.02	2.98	2.91	2.83	2.77	2.74	2.70	2.66	2.62	2.58	2.54
11	4.84	3.98	3.59	3.36	3.20	3.09	3.01	2.93	2.90	2.83	2.79	2.72	2.65	2.61	2.57	2.53	2.49	2.45	2.40
12	4.73	3.89	3.49	3.26	3.11	3.00	2.91	2.83	2.80	2.75	2.69	2.62	2.54	2.51	2.47	2.43	2.38	2.34	2.30
13	4.67	3.81	3.41	3.18	3.03	2.92	2.83	2.77	2.71	2.67	2.60	2.53	2.46	2.41	2.34	2.30	2.25	2.21	2.17
14	4.60	3.74	3.34	3.11	2.96	2.83	2.76	2.70	2.65	2.60	2.53	2.46	2.39	2.33	2.27	2.21	2.16	2.12	2.08
15	4.54	3.68	3.29	3.06	2.90	2.79	2.71	2.64	2.59	2.54	2.48	2.40	2.33	2.29	2.25	2.20	2.16	2.11	2.07
16	4.49	3.63	3.24	3.01	2.85	2.74	2.66	2.59	2.54	2.49	2.42	2.35	2.28	2.24	2.19	2.15	2.11	2.06	2.01
17	4.45	3.59	3.20	2.96	2.81	2.70	2.61	2.53	2.49	2.43	2.38	2.31	2.23	2.19	2.15	2.10	2.06	2.01	1.96
18	4.41	3.53	3.16	2.93	2.77	2.66	2.58	2.51	2.46	2.41	2.34	2.27	2.19	2.15	2.11	2.07	2.01	1.97	1.92
19	4.38	3.52	3.13	2.90	2.74	2.63	2.54	2.48	2.42	2.35	2.29	2.23	2.16	2.11	2.07	2.01	1.98	1.93	1.88
20	4.35	3.49	3.10	2.87	2.71	2.60	2.51	2.45	2.39	2.35	2.28	2.20	2.12	2.08	2.04	1.99	1.95	1.90	1.84
21	4.32	3.47	3.07	2.84	2.68	2.57	2.49	2.42	2.37	2.32	2.25	2.18	2.10	2.05	2.01	1.96	1.92	1.87	1.81
22	4.30	3.44	3.05	2.82	2.66	2.55	2.46	2.40	2.34	2.29	2.23	2.15	2.07	2.03	1.98	1.94	1.89	1.86	1.81
23	4.28	3.42	3.03	2.80	2.64	2.53	2.44	2.37	2.32	2.27	2.20	2.13	2.05	2.01	1.96	1.91	1.86	1.81	1.76
24	4.26	3.40	3.01	2.78	2.62	2.51	2.42	2.36	2.30	2.25	2.18	2.11	2.03	1.98	1.94	1.89	1.84	1.79	1.73
25	4.24	3.39	2.99	2.76	2.60	2.49	2.40	2.34	2.28	2.24	2.16	2.09	2.01	1.96	1.92	1.87	1.82	1.77	1.71
26	4.21	3.37	2.98	2.74	2.59	2.47	2.32	2.27	2.22	2.15	2.07	1.99	1.93	1.90	1.85	1.80	1.75	1.69	1.63
27	4.21	3.35	2.96	2.73	2.57	2.46	2.37	2.29	2.21	2.15	2.07	2.01	1.96	1.91	1.87	1.84	1.79	1.73	1.67
28	4.20	3.34	2.95	2.71	2.56	2.43	2.34	2.26	2.19	2.12	2.04	1.96	1.91	1.87	1.82	1.77	1.71	1.65	1.60
29	4.18	3.33	2.93	2.70	2.55	2.43	2.33	2.26	2.18	2.11	2.03	1.94	1.89	1.85	1.81	1.75	1.70	1.64	1.59
30	4.17	3.32	2.92	2.69	2.53	2.42	2.33	2.27	2.21	2.16	2.09	2.01	1.93	1.89	1.84	1.79	1.74	1.68	1.62
40	4.08	2.84	2.61	2.43	2.34	2.23	2.17	2.12	2.08	2.00	1.92	1.84	1.74	1.69	1.64	1.58	1.51	1.47	1.39
60	4.00	2.53	2.25	2.17	2.09	2.02	1.96	1.91	1.83	1.75	1.65	1.59	1.53	1.47	1.40	1.33	1.25	1.18	1.00
120	3.92	2.45	2.29	2.17	2.09	2.02	1.94	1.88	1.75	1.66	1.59	1.51	1.42	1.33	1.25	1.18	1.11	1.02	0.90
240	3.84	2.37	2.10	2.01	1.94	1.88	1.75	1.67	1.57	1.46	1.39	1.32	1.22	1.12	1.02	0.90	0.80	0.70	0.60